

Wall friction in confined flows of anisotropic particles: a unified scaling law

Antonio POL, Riccardo ARTONI, <u>Patrick RICHARD</u> GPEM, MAST, Université Gustave Eiffel, 44344 Bouguenais, France patrick.richard@univ-eiffel.fr

Introduction

Interactions of flowing granular media with flat and frictional boundaries is frequent

- Nonlocal effects
- Possible heterogeneity (static, creeplike, and shear localization regions)

understanding the behavior at interfaces is fundamental for a full 3D rheological model of granular flows.

Here, we study the effective friction at lateral flat frictional walls in a confined and shear-driven dense granular flow composed of shape anisotropic particles.

Numerical setup



- Rectangular cuboid ($L_x = 20a$ and $L_y = 10d$, L_z variable with a and d the max. and the min. axis of a particle)
- PBC in flow (x-) direction, gravity
- Two flat but frictional sidewalls
- Top and a bottom : bumpy walls (regular triangular mesh of spheres of diameter d with a spacing of 1.5d)
 ✓ The bottom wall moves at a fixed velocity V
 - \checkmark The top wall is fixed in the x- and y-directions but can freely move in the z-direction
- Normal forces : spring dashpot
- Tangential forces : spring, the displacement is limited a Coulomb plastic condition with a friction coefficient μ_{pp}
- Particle/sidewall contact treated in the same manner but with a friction coefficient μ_{pw}

Kinematics

• Shear localization at the top(bottom) for low (high) sidewall friction



Rescaled velocity profile (by considering top or bottom localization)

Top $z^* = z/d$ $v^* = v_x/(V - v_w)$ Bottom $z^* = (L_z - z)/d$ $v^* = (V - v_x)/(V - v_w)$ v_w : slip velocity at the wall

Velocity decay length almost unaffected by particles' shape

- Higher granular temperature, T, in the region where the shear localizes, independently of the flow pattern and the particle shape
- Particle shape: a negligible impact on the granular temp. esp. for zone of shear localization. Some differences far from the latter.

 μ_{pw} = 0.3 (solid lines) μ_{pw} = 0.05 (dashed lines)



Mean angular velocity \$\overline{\overline{O}_y\$ systematically \$\gamma\$ with \$\alpha\$ particle elongation
 Rotations' frustrations by particle shape is even stronger for \$\overline{O}_z\$ (rolling comp. with respect to the wall) \$\overline{O}\$ shape anisotropy hinders rolling
 The ratio of the angular velocity fluctuations to the mean angular velocity :

$$\sqrt{\langle \omega_z'^2 \rangle} = \sqrt{\langle (\omega_z - \langle \omega_z \rangle)^2 \rangle} / \overline{\omega}_z$$

strongly depends on particles' shape



Effective wall friction $\mu_w^x = \langle F_x \rangle / \langle F_y \rangle$ $\mu_w^z = \langle F_z \rangle / \langle F_y \rangle$

- Shear localizes at the bottom → the wall friction is partially mobilized in the flow direction
- Shear localizes at the top $ightarrow \mu^{\chi}_w$ is minimum in the shear region
- Increasing Ly \rightarrow higher mobilization of the effective sidewall friction
- The
 ¬ of friction mobilization with Ly is evidently related to the progressive reduction of the slowly (creeplike) moving zone





Also, it remains valid for confined free surface flows

Conclusions

- Particle shape mainly affects the angular velocity profiles both spinning and rolling motions being frustrated.
- Particle elongation also affects effective wall friction \rightarrow elongated particles show less friction weakening at the wall than more isotropic particles.
- In dense granular flows the effective friction at flat interfaces scales according to a balance between sliding and angular motion of the particles.
- Three regimes have been identified: pure sliding, no-slip-pure rolling, sliding and rolling coupling





